

Generalization of scattering problem in a quasi 1D

①

We consider a device connected to the left and right leads as depicted below.
(Lead 1)
(Lead 2)



It is assumed that electrons flow steadily from the left to right. Then, the time-dependent Schrödinger equation can be reduced to the following form.

$$\begin{pmatrix} H_1 & \tau_1 & 0 \\ \tau_1^\dagger & H_D & \tau_2^\dagger \\ 0 & \tau_2 & H_2 \end{pmatrix} \begin{pmatrix} |\psi_1\rangle \\ |\psi_D\rangle \\ |\psi_2\rangle \end{pmatrix} = E \begin{pmatrix} |\psi_1\rangle \\ |\psi_D\rangle \\ |\psi_2\rangle \end{pmatrix} \quad \dots \dots (1)$$

$H_1, H_D, H_2, \tau_1, \tau_2$ are all matrices

At the beginning, we assume that the Schrödinger eq. of the isolated lead 1 is solved as

$$H_1 |\phi_{in}\rangle = E |\phi_{in}\rangle \quad \dots \dots (2)$$

Then, we consider ϕ_{in} as incident wave to the device region. In the steady state, ψ can be expressed by the sum of incident and reflected waves as

$$|\psi\rangle = \begin{pmatrix} |\psi_1\rangle \\ |\psi_D\rangle \\ |\psi_2\rangle \end{pmatrix} = |\phi_{in}\rangle + |\chi\rangle = \begin{pmatrix} |\phi_{in}\rangle + |\chi_1\rangle \\ |\chi_D\rangle \\ |\chi_2\rangle \end{pmatrix} \quad \dots \dots (3)$$

By inserting Eq. (3) into Eq. (1), we have

(2)

$$\begin{pmatrix} E-H_1 & -\tau_1 & 0 \\ -\tau_1^\dagger & E-H_d & -\tau_2^\dagger \\ 0 & -\tau_2 & E-H_2 \end{pmatrix} \begin{pmatrix} |\phi_{1n}\rangle + |\chi_1\rangle \\ |\chi_d\rangle \\ |\chi_2\rangle \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} \quad \dots (4)$$

→

$$\begin{pmatrix} E-H_1 & -\tau_1 & 0 \\ -\tau_1^\dagger & E-H_d & -\tau_2^\dagger \\ 0 & -\tau_2 & E-H_2 \end{pmatrix} \begin{pmatrix} |\chi_1\rangle \\ |\chi_d\rangle \\ |\chi_2\rangle \end{pmatrix} = \begin{pmatrix} -(E-H_1)|\phi_{1n}\rangle \\ \tau_1^\dagger |\phi_{1n}\rangle \\ 0 \end{pmatrix} \quad \dots (5)$$

From Eq. (2), we see $-(E-H_1)|\phi_{1n}\rangle = -(E-E)|\phi_{1n}\rangle = 0$.

So, we have

$$\begin{pmatrix} |\chi_1\rangle \\ |\chi_d\rangle \\ |\chi_2\rangle \end{pmatrix} = G \begin{pmatrix} 0 \\ \tau_1^\dagger |\phi_{1n}\rangle \\ 0 \end{pmatrix} \quad \dots (6)$$

$$G = \begin{pmatrix} E-H_1 & -\tau_1 & 0 \\ -\tau_1^\dagger & E-H_d & -\tau_2^\dagger \\ 0 & -\tau_2 & E-H_2 \end{pmatrix}^{-1} = \begin{pmatrix} G_{11} & G_{1d} & G_{12} \\ G_{d1} & G_d & G_{d2} \\ G_{21} & G_{2d} & G_2 \end{pmatrix} \quad \dots (7)$$

From the second row in Eq. (6), we obtain

$$|\chi_d\rangle = G_d \tau_1^\dagger |\phi_{1n}\rangle = |\psi_d\rangle \quad \dots (8)$$

From the third row of Eq. (4), we have

③

$$(E - H_2) |\chi_2\rangle = \tau_2 |\chi_d\rangle$$

$$g_2 = (E - H_2)^{-1}$$

Note $g_2 \neq G_2$.

$$|\chi_2\rangle = (E - H_2)^{-1} \tau_2 |\chi_d\rangle = g_2 \tau_2 |\chi_d\rangle \quad \dots (9)$$

Inserting Eq. (8) into Eq. (9), we obtain

$$|\chi_2\rangle = g_2 \tau_2 G_d \tau_1^\dagger |\phi_{in}\rangle = |\psi_2\rangle \quad \dots (10)$$

From the first row of Eq. (5), we have

$$(E - H_1) |\chi_1\rangle = \tau_1 |\chi_d\rangle$$

$$g_1 = (E - H_1)^{-1}$$

$$|\chi_1\rangle = (E - H_1)^{-1} \tau_1 |\chi_d\rangle = g_1 \tau_1 |\chi_d\rangle \quad \dots (11)$$

Inserting Eq. (8) into Eq. (11) yields the following relation.

$$|\chi_1\rangle = g_1 \tau_1 G_d \tau_1^\dagger |\phi_{in}\rangle \quad \dots (12)$$

From Eqs. (8), (10), and (12), we obtain

$$|\psi_1\rangle = (1 + g_1 \tau_1 G_d \tau_1^\dagger) |\phi_{in}\rangle$$

$$|\psi_d\rangle = G_d \tau_1^\dagger |\phi_{in}\rangle \quad \dots (13)$$

$$|\psi_2\rangle = g_2 \tau_2 G_d \tau_1^\dagger |\phi_{in}\rangle$$

We see that ψ can be expressed by the incident wave ϕ_{in} .

If the scattering process occurs independently, we should consider the scattering process from the lead 2 to lead 1 equally.

Charge density in the device

(4)

From Eq. (13), we see that the wave function $\Psi_{d,n}^{(1)} (= \Psi_d)$ is contributed by the incident wave ϕ_{in} from the lead 1.

So, the density operator of the device region can be defined by

$$\begin{aligned}
 \hat{\rho}_d^{(1)} &= \int_{-\infty}^{\infty} dE \sum_n f(E, \mu_1) \delta(E - E_n) |\Psi_{d,n}^{(1)}\rangle \langle \Psi_{d,n}^{(1)}| \\
 &= \int_{-\infty}^{\infty} dE f(E, \mu_1) \sum_n \delta(E - E_n) \underbrace{G_d \tau_1^\dagger |\phi_{in}\rangle \langle \phi_{in}| \tau_1 G_d^\dagger}_{\text{Eq. (13)}} \quad \frac{a_1}{2\pi} \\
 &= \int_{-\infty}^{\infty} dE f(E, \mu_1) G_d \tau_1^\dagger \left[\sum_n \delta(E - E_n) |\phi_{in}\rangle \langle \phi_{in}| \right] \tau_1 G_d^\dagger \\
 &= \int_{-\infty}^{\infty} dE f(E, \mu_1) G_d \tau_1^\dagger \frac{a_1}{2\pi} \tau_1 G_d^\dagger \quad \text{----- (14)}
 \end{aligned}$$

By defining $\Gamma_1 = \tau_1^\dagger a_1 \tau_1$ ----- (15)

we rewrite Eq. (14) as

$$\hat{\rho}_d^{(1)} = \frac{1}{2\pi} \int_{-\infty}^{\infty} dE f(E, \mu_1) G_d \Gamma_1 G_d^\dagger \quad \text{----- (16)}$$

This is called Non-Equilibrium Green's Function (NEGF).

The matrix elements of $\hat{\rho}_d^{(1)}$ are evaluated by $\langle l | \hat{\rho}_d^{(1)} | m \rangle$ where $|l\rangle$ and $|m\rangle$ are basis functions in the device region.

By considering all the contributions from all the leads connected to the device, we obtain

Spin degeneracy \rightarrow

$$\hat{\rho} = \frac{2}{2\pi} \int_{-\infty}^{\infty} dE \left[\sum_i f(E, \mu_i) G_d \Gamma_i G_d^\dagger \right] \quad \text{----- (17)}$$

Current through the device

(5)

In the non-equilibrium steady state the probability density of the device region is conserved. We evaluate the flux of the probability density using the time-dependent Schrödinger equation as

$$i\hbar \frac{\partial}{\partial t} \begin{pmatrix} |\psi_1\rangle \\ |\psi_d\rangle \\ |\psi_2\rangle \end{pmatrix} = \begin{pmatrix} H_1 & \tau_1 & 0 \\ \tau_1^\dagger & H_d & \tau_2^\dagger \\ 0 & \tau_2 & H_2 \end{pmatrix} \begin{pmatrix} |\psi_1\rangle \\ |\psi_d\rangle \\ |\psi_2\rangle \end{pmatrix} \quad \dots\dots (18)$$

The time evolution of the integrated probability density is given by

$$\begin{aligned} \frac{\partial}{\partial t} \langle \psi_d | \psi_d \rangle &= \frac{\partial \langle \psi_d |}{\partial t} |\psi_d\rangle + \langle \psi_d | \frac{\partial |\psi_d\rangle}{\partial t} \\ &= \frac{i}{\hbar} \left[\langle \psi_2 | \tau_2 + \langle \psi_d | H_d + \langle \psi_1 | \tau_1 \right] |\psi_d\rangle \quad \leftarrow \text{From Eq. (18)} \\ &\quad - \frac{i}{\hbar} \langle \psi_d | \left[\tau_1^\dagger |\psi_1\rangle + H_d |\psi_d\rangle + \tau_2^\dagger |\psi_2\rangle \right] \\ &= \frac{i}{\hbar} \left[\left(\langle \psi_1 | \tau_1 | \psi_d \rangle - \langle \psi_d | \tau_1^\dagger | \psi_1 \rangle \right) + \left(\langle \psi_2 | \tau_2 | \psi_d \rangle - \langle \psi_d | \tau_2^\dagger | \psi_2 \rangle \right) \right] \end{aligned} \quad \dots\dots (19)$$

Each term in Eq. (19) can be regarded as the contribution from each lead R .

This is purely imaginary.

The flow of current is opposite to that of electron

$$i_R = - \frac{ie}{\hbar} \left(\langle \psi_R | \tau_R | \psi_d \rangle - \langle \psi_d | \tau_R^\dagger | \psi_R \rangle \right) \quad \dots\dots (20)$$

Because of conservation of probability density,

$$\text{we have} \quad \sum_R i_R = 0 \quad \dots\dots (21)$$

(6)

From the condition of Eq. (21) for the steady state,

we obtain

$$i_2 = -i_1 \quad \text{----- (22)}$$

So, the current from the lead 1 to the lead 2

can be calculated from i_2 .



$$i_{1 \rightarrow 2} = i_2 = -\frac{ie}{\hbar} \left(\langle \psi_2 | \tau_2 | \psi_d \rangle - \langle \psi_d | \tau_2^\dagger | \psi_2 \rangle \right) \quad \text{----- (23)}$$

Using Eq. (13), one can calculate as

$$i_{1 \rightarrow 2} = -\frac{ie}{\hbar} \left(\langle \phi_{1n} | \tau_1 G_d^\dagger \tau_2^\dagger g_2^\dagger \tau_2 G_d \tau_1^\dagger | \phi_{1n} \rangle - \langle \phi_{1n} | \tau_1 G_d^\dagger \tau_2^\dagger g_2 \tau_2 G_d \tau_1^\dagger | \phi_{1n} \rangle \right)$$

$$= -\frac{ie}{\hbar} \langle \phi_{1n} | \tau_1 G_d^\dagger \tau_2^\dagger (g_2^\dagger - g_2) \tau_2 G_d \tau_1^\dagger | \phi_{1n} \rangle \quad \text{----- (24)}$$

By defining

$$\Gamma_2 = -i \tau_2^\dagger (g_2^\dagger - g_2) \tau_2 \quad \text{----- (25)}$$

Eq. (24) can be rewritten as

$$i_{1 \rightarrow 2} = \frac{e}{\hbar} \langle \phi_{1n} | \tau_1 G_d^\dagger \Gamma_2 G_d \tau_1^\dagger | \phi_{1n} \rangle \quad \text{----- (26)}$$

★ Equivalence of Eqs. (15) and (25).

$$\text{Noting } g_R(E) = \sum_n \frac{|\phi_{Rn}\rangle \langle \phi_{Rn}|}{E - E_n} \quad \text{----- (27)}$$

$$\begin{aligned} g_R(E) - g_R^\dagger(E) &= \sum_n |\phi_{Rn}\rangle \langle \phi_{Rn}| \left(\frac{1}{E - E_n + i\eta} - \frac{1}{E - E_n - i\eta} \right) \\ &= \sum_n |\phi_{Rn}\rangle \langle \phi_{Rn}| \left(\frac{-2i\eta}{(E - E_n)^2 + \eta^2} \right) \xrightarrow{\eta \rightarrow 0} \sum_n |\phi_{Rn}\rangle \langle \phi_{Rn}| (-2i\pi \delta(E - E_n)) \end{aligned}$$

So, one can calculate as

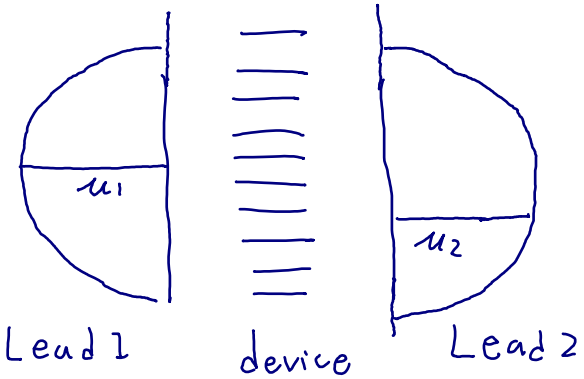
$$\Gamma_R = -i \tau_R^\dagger (g_R^\dagger - g_R) \tau_R = \tau_R^\dagger \left(\sum_n 2\pi \delta(E - E_n) |\phi_{Rn}\rangle \langle \phi_{Rn}| \right) \tau_R$$

Thus, we see the definition of Eq. (25) is equivalent to Eq. (15).

Now we consider all the contributions from the incident wave ϕ_{in} to the current. Eq. (26)

$$\begin{aligned}
 I_{1 \rightarrow 2} &= 2 \frac{e}{\hbar} \int_{-\infty}^{\infty} dE f(E, \mu_1) \sum_n \delta(E - E_n) \langle \phi_{in} | \tau_1 G_d^\dagger \Gamma_2 G_d \tau_1^\dagger | \phi_{in} \rangle \\
 &= \frac{2e}{\hbar} \int_{-\infty}^{\infty} dE f(E, \mu_1) \sum_n \sum_m \delta(E - E_n) \langle \phi_{in} | \tau_1 | m \rangle \langle m | G_d^\dagger \Gamma_2 G_d \tau_1^\dagger | \phi_{in} \rangle \\
 &= \frac{2e}{\hbar} \int_{-\infty}^{\infty} dE f(E, \mu_1) \sum_m \langle m | G_d^\dagger \Gamma_2 G_d \tau_1^\dagger \left(\sum_n \delta(E - E_n) | \phi_{in} \rangle \langle \phi_{in} | \right) \tau_1 | m \rangle \\
 &= \frac{2e}{\hbar} \int_{-\infty}^{\infty} dE f(E, \mu_1) \sum_m \langle m | G_d^\dagger \Gamma_2 G_d \tau_1^\dagger \frac{\alpha_1}{2\pi} \tau_1 | m \rangle \\
 &= \frac{e}{\pi \hbar} \int_{-\infty}^{\infty} dE f(E, \mu_1) \text{Tr} \left(G_d^\dagger \Gamma_2 G_d \Gamma_1 \right) \dots \dots (28)
 \end{aligned}$$

By considering the following situation:



Transmission
 $T(E) = \text{Tr} (G_d^\dagger \Gamma_2 G_d \Gamma_1)$ (30)
 The expressions of Eqs. (29) and (30) are called Landauer formula.

it is found that $I_{1 \rightarrow 2}$ is regarded the current from the lead 1 to the lead 2. As well we need to take account of the current from the lead 2 to lead 1.

Since we assume the steady state of Eq. (22), we have the total current as

$$\boxed{I = \frac{2e}{\hbar} \int_{-\infty}^{\infty} dE (f(E, \mu_1) - f(E, \mu_2)) \text{Tr} (G_d^\dagger \Gamma_2 G_d \Gamma_1) \dots \dots (29)}$$

Evaluation of G_d

The Green's function G_d of the device region is evaluated by Eq.(17). By definition, we have

$$\begin{pmatrix} E-H_1 & -\tau_1 & 0 \\ -\tau_1^\dagger & E-H_d & -\tau_2^\dagger \\ 0 & -\tau_2 & E-H_2 \end{pmatrix} \begin{pmatrix} G_1 & G_{1d} & G_{12} \\ G_{d1} & G_d & G_{d2} \\ G_{21} & G_{2d} & G_2 \end{pmatrix} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \quad \dots (31)$$

row 1 \times column 2

$$(E-H_1) G_{1d} - \tau_1 G_d = 0 \quad \dots (32)$$

row 2 \times column 2

$$-\tau_1^\dagger G_{1d} + (E-H_d) G_d - \tau_2^\dagger G_{2d} = 1 \quad \dots (33)$$

row 3 \times column 2

$$-\tau_2 G_d + (E-H_2) G_{2d} = 0 \quad \dots (34)$$

From (32), we have

$$G_{1d} = (E-H_1)^{-1} \tau_1 G_d = g_1 \tau_1 G_d \quad \dots (35)$$

From (34), we have

$$G_{2d} = (E-H_2)^{-1} \tau_2 G_d = g_2 \tau_2 G_d \quad \dots (36)$$

Inserting Eqs. (35) and (36) into Eq. (33), we obtain

$$-\tau_1^\dagger g_1 \tau_1 G_d + (E-H_d) G_d - \tau_2^\dagger g_2 \tau_2 G_d = 1$$

$$(E-H_d - \Sigma_1 - \Sigma_2) G_d = 1$$

$$G_d = (E-H_d - \Sigma_1 - \Sigma_2)^{-1} \quad \dots (37)$$

where

$$\Sigma_1 = \tau_1^\dagger g_1 \tau_1 \quad \dots (38)$$

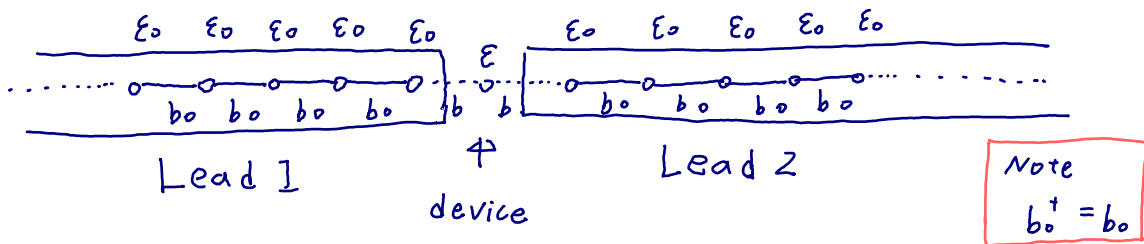
$$\Sigma_2 = \tau_2^\dagger g_2 \tau_2 \quad \dots (39)$$

g_1 and g_2 are called surface Green's function.

Σ_1 and Σ_2 are called self-energy.

An example: linear chain model

Let's consider a linear chain model as shown below.



To calculate the surface Green functions of the leads 1 and 2, we employ the recursion method discussed in "Recursion_method.pdf".

From the page 13 in the lecture notes, we have

$$g_1(z) = g_2(z) = \frac{z - \epsilon_0 - \sqrt{(z - \epsilon_0)^2 - 4b_0^2}}{2b_0^2} \quad \dots \quad (40)$$

The self-energies of Eqs. (38) and (39) are given by

$$\Sigma_1(z) = \Sigma_2(z) = b^2 g_1(z) = \frac{b^2}{2b_0^2} (z - \epsilon_0 - \sqrt{(z - \epsilon_0)^2 - 4b_0^2}) \quad \dots \quad (41)$$

The Green function of Eq. (37) is found to be

$$G_d(z) = \left[z - \epsilon - \frac{b^2}{b_0^2} (z - \epsilon_0 - \sqrt{(z - \epsilon_0)^2 - 4b_0^2}) \right]^{-1} \quad \dots \quad (42)$$

Also, Γ_1 and Γ_2 are calculated as

$$\Gamma_1 = \Gamma_2 = i b (g_1 - g_1^\dagger) b = \frac{i b^2}{2b_0^2} (z - \cancel{\epsilon_0} - \sqrt{(z - \epsilon_0)^2 - 4b_0^2} - z^* + \cancel{\epsilon_0} + \sqrt{(z^* - \epsilon_0)^2 - 4b_0^2}) \quad \dots \quad (43)$$

Thus, the transmission is given by

$$T(E) = \text{Tr} \left(\underset{\substack{\uparrow \\ (42)}}{G_d^\dagger} \underset{\substack{\uparrow \\ (43)}}{\Gamma_2} \underset{\substack{\uparrow \\ (42)}}{G_d} \underset{\substack{\uparrow \\ (43)}}{\Gamma_1} \right) \quad \dots \quad (44)$$

In case that $\epsilon = \epsilon_0$ and $h = h_0$, we have

$$G_d(z) = \frac{1}{\sqrt{(z - \epsilon_0)^2 - 4b^2}} \quad \dots\dots (45)$$

This is equivalent to Eq. (28) in the page 16 of lecture notes 2.

Taking $z = E + i\eta$ ($\eta \rightarrow 0$), G_d becomes

$$G_d(E + i\eta) = \frac{1}{\sqrt{(E - \epsilon_0)^2 - \eta^2 + 2i\eta(E - \epsilon_0) - 4b^2}}$$

For $(E - \epsilon_0)^2 - 4b_0^2 < 0 \rightarrow \epsilon_0 - 2|b_0| < E < \epsilon_0 + 2|b_0|$

$$\text{Im } G_d = -\frac{1}{\sqrt{4b_0^2 - (E - \epsilon_0)^2}}, \quad \text{Re } G_d = 0 \quad \dots\dots (46)$$

For $E < \epsilon_0 - 2|b_0|$, $\epsilon_0 + 2|b_0| < E$

$$\text{Im } G_d = 0, \quad \text{Re } G_d = \frac{1}{\sqrt{(E - \epsilon_0)^2 - 4b_0^2}} \quad \dots\dots (47)$$

Noting for $\eta \rightarrow 0$

$$P_1 = P_2 = ib^2(g_1 - g_1^+) = -2b^2 \text{Im } g_1 = \begin{cases} \sqrt{4b_0^2 - (E - \epsilon_0)^2} & \epsilon_0 - 2|b_0| < E < \epsilon_0 + 2|b_0| \\ 0 & \text{else} \end{cases} \quad \dots\dots (48)$$

From Eqs. (46) - (48), we obtain the transmission.

$$T(E) = \text{Tr} (G_d^\dagger P_2 G_d P_1) = (-i) \times i \left(\frac{1}{\sqrt{4b_0^2 - (E - \epsilon_0)^2}} \right)^2 \times \left(\sqrt{4b_0^2 - (E - \epsilon_0)^2} \right)^2 = 1$$

for $\epsilon_0 - 2|b_0| < E < \epsilon_0 + 2|b_0|$

Other wise $\dots\dots\dots (49)$

$$T(E) = 0$$

Conductance quantum

Let us start Eq. (29).

$$I = \frac{2e}{h} \int_{-\infty}^{\infty} dE T(E) [f(E-\mu_1) - f(E-\mu_2)] \dots (29)$$

Our purpose here is to find a relation

$$I = \frac{V}{R} = VG \dots (50)$$

where V is the source-drain bias voltage, R resistance,

and $G \equiv \frac{1}{R}$ conductance. To derive Eq. (50) based on Eq. (29),

we consider a case that $\mu_1 = \mu_2 + eV = \mu + eV$ with a tiny V .

Then, Eq. (29) can be approximated by

$$\begin{aligned} I &\simeq \frac{2e}{h} \int_{-\infty}^{\infty} dE \left[T(\mu) + \left. \frac{\partial T(E)}{\partial E} \right|_{E=\mu} (E-\mu) \right] \left[f(E-\mu) + \left. \frac{\partial f(E-\mu+eV)}{\partial V} \right|_{V=0} V - f(E-\mu) \right] \\ &= \frac{2e}{h} \left[\int_{-\infty}^{\infty} dE T(\mu) \frac{\partial f(E-\mu+eV)}{\partial V} V + \int_{-\infty}^{\infty} dE \frac{\partial T(E)}{\partial E} (E-\mu) \frac{\partial f(E-\mu+eV)}{\partial V} V \right] \end{aligned}$$

Noting $\frac{\partial f(E-\mu+eV)}{\partial V} = -e \frac{\partial f(E-\mu+eV)}{\partial E} \xrightarrow{V \rightarrow 0} e \delta(E-\mu)$ (51)

Eq. (51) becomes

$$I = \frac{2e^2}{h} T(\mu) V \int_{-\infty}^{\infty} dE \delta(E-\mu) = V \left(T(\mu) \frac{2e^2}{h} \right) \dots (52)$$

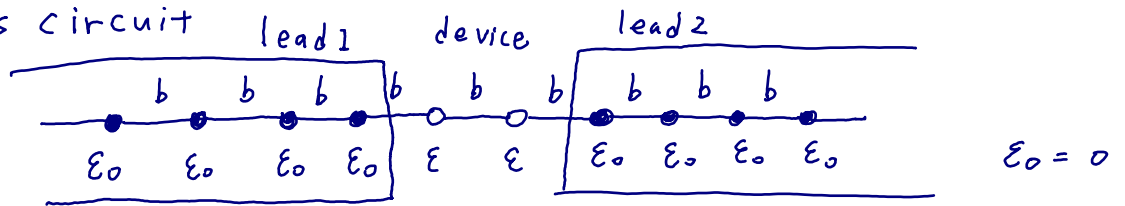
Compared to Eq. (50), we obtain

G_0 is called $G = T(\mu) G_0 \dots (53)$

conductance quantum $G_0 = \frac{2e^2}{h} \dots (54)$

Conductance of series and parallel circuits

(a) series circuit



As well as the lecture notes 2 and 13, the surface Green functions are given by

$$g_1(z) = g_2(z) = \frac{z - \sqrt{z^2 - 4b^2}}{2b^2} \quad \dots \dots (1)$$

The self-energies can be calculated as

$$\Sigma_1(z) = \begin{pmatrix} b \\ 0 \end{pmatrix} g_1(z) \begin{pmatrix} b & 0 \end{pmatrix} = \begin{pmatrix} b^2 g_1(z) & 0 \\ 0 & 0 \end{pmatrix} \quad \dots \dots (2)$$

$$\Sigma_2(z) = \begin{pmatrix} 0 \\ b \end{pmatrix} g_2(z) \begin{pmatrix} 0 & b \end{pmatrix} = \begin{pmatrix} 0 & 0 \\ 0 & b^2 g_2(z) \end{pmatrix} \quad \dots \dots (3)$$

The Green function of the device region is given by

$$G_d(z) = (z - H_d - \Sigma_1(z) - \Sigma_2(z))^{-1}$$

$$= \begin{pmatrix} z - \varepsilon - \frac{1}{2}(z - \sqrt{z^2 - 4b^2}) & -b \\ -b & z - \varepsilon - \frac{1}{2}(z - \sqrt{z^2 - 4b^2}) \end{pmatrix}^{-1} = \begin{pmatrix} A & B \\ B & A \end{pmatrix}^{-1} = \frac{1}{A^2 - B^2} \begin{pmatrix} A & -B \\ -B & A \end{pmatrix}$$

$$= \frac{1}{C} \begin{pmatrix} z - \varepsilon - \frac{1}{2}(z - \sqrt{z^2 - 4b^2}) & b \\ b & z - \varepsilon - \frac{1}{2}(z - \sqrt{z^2 - 4b^2}) \end{pmatrix} \quad C = \left[z - \varepsilon - \frac{1}{2}(z - \sqrt{z^2 - 4b^2}) \right]^2 - b^2 \quad \dots \dots (5)$$

$$= \begin{pmatrix} \alpha & \beta \\ \beta & \alpha \end{pmatrix} \quad \dots \dots (4)$$

Γ_1 and Γ_2 can be calculated as

$$\Gamma_1 = i \tau_1^\dagger (g_1 - g_1^\dagger) \tau_1 = i \begin{pmatrix} b \\ 0 \end{pmatrix} 2i \text{Im} g_1 \begin{pmatrix} b & 0 \end{pmatrix}$$

$$= -2b^2 \text{Im} g_1 \begin{pmatrix} 1 & 0 \\ 0 & 0 \end{pmatrix} = \sqrt{4b^2 - E^2} \begin{pmatrix} 1 & 0 \\ 0 & 0 \end{pmatrix}$$

$$\Gamma_2 = i \tau_2^\dagger (g_2 - g_2^\dagger) \tau_2 = i \begin{pmatrix} 0 \\ b \end{pmatrix} 2i \text{Im} g_2 \begin{pmatrix} 0 & b \end{pmatrix}$$

$$= -2b^2 \text{Im} g_2 \begin{pmatrix} 0 & 0 \\ 0 & 1 \end{pmatrix} = \sqrt{4b^2 - E^2} \begin{pmatrix} 0 & 0 \\ 0 & 1 \end{pmatrix}$$

for $-2|b| < E < 2|b|$ ----- (6)

otherwise, they are zero.

Then, one can calculate the transmission as

$$T(E) = \text{Tr} (G_d^\dagger \Gamma_2 G_d \Gamma_1)$$

$$= (4b^2 - E^2) \text{Tr} \left[\begin{pmatrix} \alpha^* & \beta^* \\ \beta^* & \alpha^* \end{pmatrix} \begin{pmatrix} 0 & 0 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} \alpha & \beta \\ \beta & \alpha \end{pmatrix} \begin{pmatrix} 1 & 0 \\ 0 & 0 \end{pmatrix} \right]$$

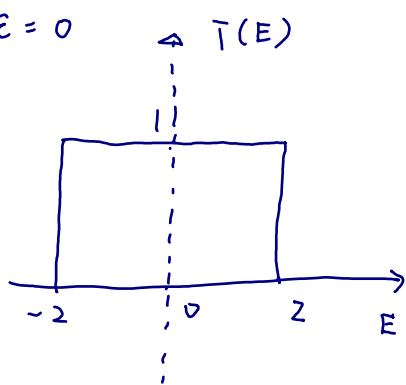
$$= (4b^2 - E^2) \text{Tr} \left[\begin{pmatrix} 0 & \beta^* \\ 0 & \alpha^* \end{pmatrix} \begin{pmatrix} \alpha & 0 \\ \beta & 0 \end{pmatrix} \right] = (4b^2 - E^2) \text{Tr} \begin{pmatrix} \beta^* \beta & 0 \\ \alpha^* \beta & 0 \end{pmatrix}$$

$$= (4b^2 - E^2) \beta^* \beta$$

$$= (4b^2 - E^2) \times b^2 \times \frac{1}{c^* c} \text{ ----- (7)}$$

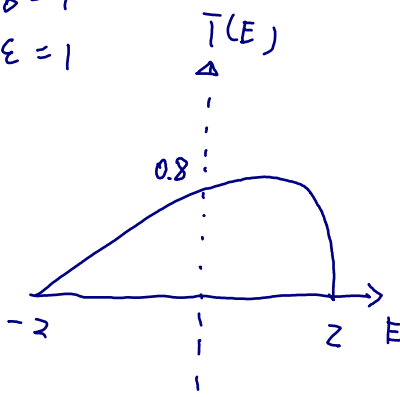
$b=1$

$E=0$



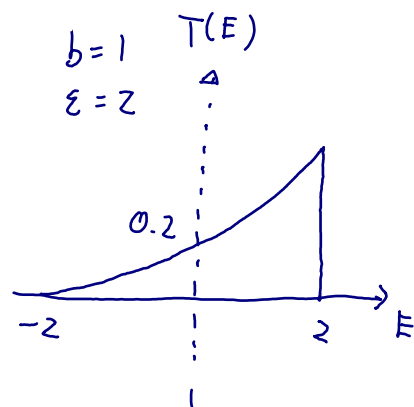
$b=1$

$E=1$



$b=1$

$E=2$



Noting that $T(E)$ at $E=0$ is the conductance, we have C^*C at $E=0$ as

$$C^*C (E=0) = [(-\epsilon + ib)^2 - b^2][(-\epsilon - ib)^2 - b^2]$$

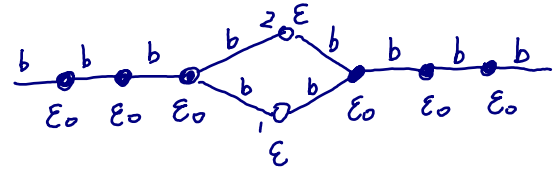
$$= 4b^4 + \epsilon^4 \quad \text{----- (8)}$$

Thus, we obtain from Eqs. (7) and (8)

$$G = 4b^2 \times b^2 \times \frac{1}{C^*C (E=0)}$$

$$= \frac{4b^4}{4b^4 + \epsilon^4} \quad \text{in } G_0 \quad \text{----- (9)}$$

(b) parallel circuit



The surface Green functions are given by Eqs. (1).

The self-energies can be calculated as

$$\Sigma_1(z) = \begin{pmatrix} b \\ b \end{pmatrix} g_1(z) \begin{pmatrix} b & b \end{pmatrix} = b^2 g_1(z) \begin{pmatrix} 1 & 1 \\ 1 & 1 \end{pmatrix} \quad \text{----- (10)}$$

$$\Sigma_2(z) = \begin{pmatrix} b \\ b \end{pmatrix} g_2(z) \begin{pmatrix} b & b \end{pmatrix} = b^2 g_2(z) \begin{pmatrix} 1 & 1 \\ 1 & 1 \end{pmatrix} \quad \text{--- (11)}$$

The Green function of the device region is given by

$$G_d(z) = (zI - H_d - \Sigma_1 - \Sigma_2)^{-1}$$

$$= \begin{pmatrix} \cancel{z} - \epsilon - \cancel{z} + \sqrt{z^2 - 4b^2} & -z + \sqrt{z^2 - 4b^2} \\ -z + \sqrt{z^2 - 4b^2} & \cancel{z} - \epsilon - \cancel{z} + \sqrt{z^2 - 4b^2} \end{pmatrix}^{-1} = \begin{pmatrix} A & B \\ B & A \end{pmatrix}^{-1} = \frac{1}{A^2 - B^2} \begin{pmatrix} A & -B \\ -B & A \end{pmatrix}$$

----- (12)

$$G_d(z) = \frac{1}{c} \begin{pmatrix} -\varepsilon + \sqrt{z^2 - 4b^2} & z - \sqrt{z^2 - 4b^2} \\ z - \sqrt{z^2 - 4b^2} & -\varepsilon + \sqrt{z^2 - 4b^2} \end{pmatrix} \dots (13)$$

$$C = (-\varepsilon + \sqrt{z^2 - 4b^2})^2 - (z - \sqrt{z^2 - 4b^2})^2 \dots (14)$$

Γ_1 and Γ_2 can be calculated as

$$\begin{aligned} \Gamma_1 &= i \tau_1^\dagger (g_1 - g_1^\dagger) \tau_1 \\ &= i \begin{pmatrix} b \\ b \end{pmatrix} z i \operatorname{Im} g_1 (b \ b) = -2b^2 \operatorname{Im} g_1 \begin{pmatrix} 1 & 1 \\ 1 & 1 \end{pmatrix} \\ &= \sqrt{4b^2 - E^2} \begin{pmatrix} 1 & 1 \\ 1 & 1 \end{pmatrix} \dots (15) \end{aligned}$$

$$\begin{aligned} \Gamma_2 &= i \tau_2^\dagger (g_2 - g_2^\dagger) \tau_2 = -2b^2 \operatorname{Im} g_2 \begin{pmatrix} 1 & 1 \\ 1 & 1 \end{pmatrix} \\ &= \sqrt{4b^2 - E^2} \begin{pmatrix} 1 & 1 \\ 1 & 1 \end{pmatrix} \dots (16) \end{aligned}$$

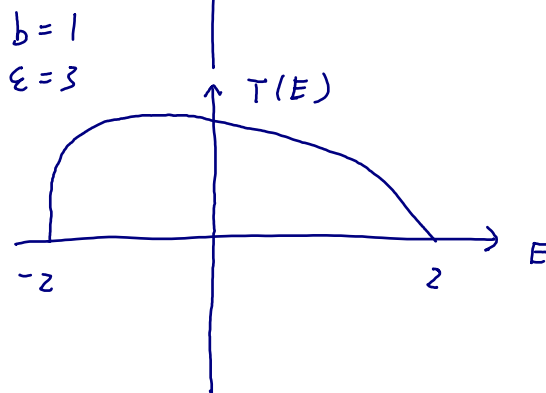
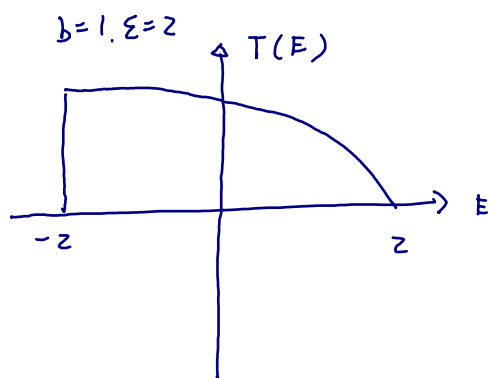
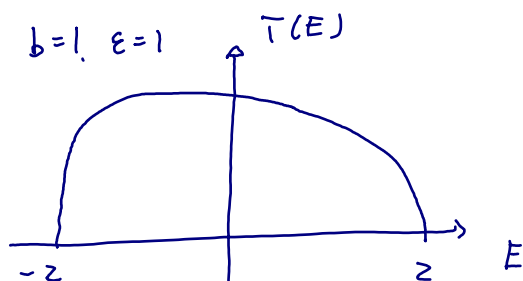
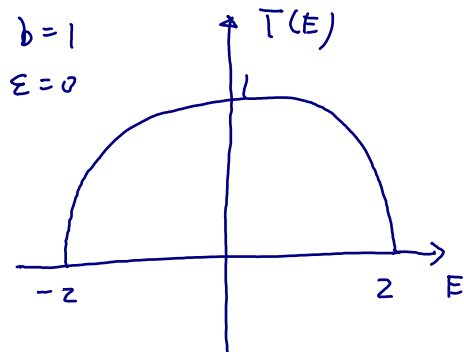
for $-2|b| < E < 2|b|$

otherwise, they are zero.

So, the transmission are given by

$$\begin{aligned} T(E) &= \operatorname{Tr} (G_d^\dagger \Gamma_2 G_d \Gamma_1) \\ &= \frac{1}{c^*c} (4b^2 - E^2) \operatorname{Tr} \left[\begin{pmatrix} -\varepsilon + \sqrt{z^{*2} - 4b^2} & z^* - \sqrt{z^{*2} - 4b^2} \\ z^* - \sqrt{z^{*2} - 4b^2} & -\varepsilon + \sqrt{z^{*2} - 4b^2} \end{pmatrix} \begin{pmatrix} 1 & 1 \\ 1 & 1 \end{pmatrix} \right. \\ &\quad \left. \times \begin{pmatrix} -\varepsilon + \sqrt{z^2 - 4b^2} & z - \sqrt{z^2 - 4b^2} \\ z - \sqrt{z^2 - 4b^2} & -\varepsilon + \sqrt{z^2 - 4b^2} \end{pmatrix} \begin{pmatrix} 1 & 1 \\ 1 & 1 \end{pmatrix} \right] \end{aligned}$$

$$T(E) = \frac{-4E^2 + 16b^2}{(\varepsilon + z - 2\sqrt{z^2 - 4b^2})(\varepsilon + z^* - 2\sqrt{z^{*2} - 4b^2})} \dots (17)$$



From Eq. (17) at $E=0$, we obtain the conductance

$$G = \frac{16b^2}{(\varepsilon - z \times z b i)(\varepsilon + z \times z b i)} = \frac{16b^2}{\varepsilon^2 + 16b^2} \dots (18)$$

in G_0

Conductance of



$$\frac{4b^2}{(-\varepsilon + 2b)^2} \dots (19)$$

Comparing with Eqs. (9), (18), and (19), we see that

Ohm's law is not valid anymore.